

Appendix T to:

A Theoretical Investigation to the Physical Constraints for Light Velocity in Empty Euclidian Space and first Consequences for Long-distance Physics.

Referred equations: (9), (12), (13), (14), (31), (34), (34a) (35)

Basic time transformation for force-free moving system

Again, a photon is considered travelling from then back to the origin of the now moving system, similar to equation (13) but now with different starting and ending locations:

$$(T.1) \quad \begin{aligned} \vec{r}_{ph}(T_1) &= \vec{d}_1 = \vec{d}(T_1) & \vec{r}_{ph}^*(T_1^*) &= 0 \\ \vec{r}_{ph}(T_m) &= \vec{r}_m & \vec{r}_{ph}^*(T_m^*) &= \vec{r}_m^* \\ \vec{r}_{ph}(T_2) &= \vec{d}_2 = \vec{d}(T_2) & \vec{r}_{ph}^*(T_2^*) &= 0 \end{aligned}$$

where \vec{r}_m is the target location and the relations between T_m , T_1 and T_2 now are, from equations (9) and (34a) with corresponding $\vec{\gamma}_m$, $\vec{\gamma}_d$:

$$(T.2) \quad \begin{aligned} \vec{\gamma}_m - \vec{r}_m &= (\vec{\gamma}_m - \vec{d}_\infty) \frac{T_1}{T_m} + \vec{d}_\infty \frac{T_{or}}{T_m} \\ \vec{\gamma}_d - \vec{r}_m &= (\vec{\gamma}_d - \vec{d}_\infty) \frac{T_2}{T_m} + \vec{d}_\infty \frac{T_{or}}{T_m} \end{aligned}$$

However, these are implicit relationships because also the $\vec{\gamma}_m$, $\vec{\gamma}_d$ depend on T_1 , T_2 respectively. Considering the top equation, travel from \vec{d}_1 to \vec{r}_m , towards $\vec{\gamma}_m$, the situation is depicted in the figure at the right. In the triangle PQR, the left side, PR, is the vector $\vec{\gamma}_m - \vec{r}_m$ and consequently the other sides must consist of the other vectors, according to their direction:

$$(T.3) \quad PQ = (\vec{\gamma}_m - \vec{d}_\infty) \frac{T_1}{T_m} \quad RQ = \vec{d}_\infty \frac{T_{or}}{T_m}$$

thus the point Q is:

$$(T.4) \quad Q = \vec{r}_m + \vec{d}_\infty \frac{T_{or}}{T_m}$$

so that the line where the P, Q and \vec{d}_∞ are located is described by:

$$(T.5) \quad \vec{r} = \vec{d}_\infty + u \left\{ \vec{r}_m - \vec{d}_\infty \left(1 - \frac{T_{or}}{T_m} \right) \right\} = \vec{d}_\infty + u (\vec{r}_m - \vec{d}_m)$$

where \vec{r} is a point on the line, u is the corresponding location on the line and $\vec{d}_m = \vec{d}_\infty (1 - T_{or}/T_m)$. Q is reached for $u = 1$ and P will be reached for an u_e where $|\vec{r}|^2 = \gamma^2$:

$$(T.6) \quad \gamma^2 = |\vec{d}_\infty + u_e (\vec{r}_m - \vec{d}_m)|^2 = d_\infty^2 + 2 u_e \vec{d}_\infty \cdot (\vec{r}_m - \vec{d}_m) + u_e^2 |\vec{r}_m - \vec{d}_m|^2$$

Note, that u_e is positive since $\vec{\gamma}_m$ and \vec{r}_m are at the same side of the x-axis. This equation is rewritten as:

$$(T.7) \quad (\gamma^2 - d_\infty^2) \left(\frac{1}{u_e} \right)^2 - \vec{d}_\infty \cdot (\vec{r}_m - \vec{d}_m) \frac{2}{u_e} - |\vec{r}_m - \vec{d}_m|^2 = 0$$

from which can be solved – note, that $\vec{d}_\infty \cdot \vec{r}_m = d_\infty x_m$ and $\vec{d}_\infty \cdot \vec{d}_m = d_\infty |d_m|$:

$$(T.8) \quad \frac{1}{u_e} (\gamma^2 - d_\infty^2) = d_\infty (x_m - |d_m|) + \sqrt{\gamma^2 |\vec{r}_m - \vec{d}_m|^2 - y_m^2 d_\infty^2}$$

where the + sign of the square root pertains since u_e is positive. PQ can be expressed as a part $u_e - 1$ of the total line piece u_e :

$$(T.9) \quad PQ = (\vec{\gamma}_m - \vec{d}_\infty) \frac{u_e - 1}{u_e}$$

so that combination with equation (T.3):

$$(T.10) \quad \frac{T_1}{T_m} = \frac{u_e - 1}{u_e} = 1 - \frac{1}{u_e}$$

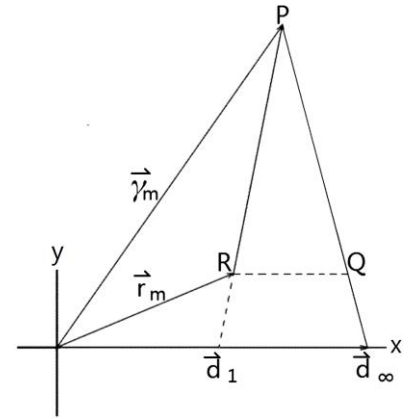
leads to, after some math:

$$(T.11) \quad \frac{T_1}{T_m} (\gamma^2 - d_\infty^2) = \gamma^2 - x_m d_\infty - d_\infty^2 \frac{T_{or}}{T_m} - \sqrt{\gamma^2 |\vec{r}_m - \vec{d}_m|^2 - y_m^2 d_\infty^2}$$

Following the same treatment for the back travel, we derive for T_2 :

$$(T.12) \quad \frac{T_2}{T_m} (\gamma^2 - d_\infty^2) = \gamma^2 - x_m d_\infty - d_\infty^2 \frac{T_{or}}{T_m} + \sqrt{\gamma^2 |\vec{r}_m - \vec{d}_m|^2 - y_m^2 d_\infty^2}$$

so that:



$$(T.13) \quad \frac{T_1 + T_2}{T_m} (\gamma^2 - d_\infty^2) = 2 \left(\gamma^2 - x_m d_\infty - d_\infty^2 \frac{T_{or}}{T_m} \right)$$

For the moving system, equation (14)

$$(14) \quad 2 T_m^* = T_1^* + T_2^*$$

remains valid – the right part of equation (T.1) is identical to that of equation (13) – so that combination with the universally valid equation (12):

$$(12) \quad T^*(x,y,T) = \Theta(x,y) T - \Delta t_{or}$$

leads to – again, the parameters T_{or} , v_{or} are left out to improve readability:

$$(T.14) \quad 2 \Theta(x_m, y_m) T_m = \Theta(d_1; 0) T_1 + \Theta(d_2; 0) T_2$$

According to Appendix M, the exact form of equation (31) is universally valid so that:

$$(T.15) \quad 2 \Theta(x_m, y_m) T_m = \Theta(0,0) \left\{ 1 - \frac{d_1 v_{or} T_{or}}{\gamma^2} \right\} T_1 + \Theta(0,0) \left\{ 1 - \frac{d_2 v_{or} T_{or}}{\gamma^2} \right\} T_2$$

Applying equation (34) for $d_1 = d(T_1)$ and $d_2 = d(T_2)$ and replacing $v_{or} T_{or}$ by d_∞ :

$$(T.16) \quad 2 \Theta(x_m, y_m) T_m = \Theta(0,0) \left\{ 1 - \frac{d_\infty^2}{\gamma^2} \left(1 - \frac{T_{or}}{T_1} \right) \right\} T_1 + \Theta(0,0) \left\{ 1 - \frac{d_\infty^2}{\gamma^2} \left(1 - \frac{T_{or}}{T_2} \right) \right\} T_2$$

$$= \Theta(0,0) \left(1 - \frac{d_\infty^2}{\gamma^2} \right) (T_1 + T_2) + 2 \Theta(0,0) \frac{d_\infty^2}{\gamma^2} T_{or}$$

so that combination with equation (T.13) gives:

$$(T.17) \quad 2 \Theta(x_m, y_m) T_m = \Theta(0,0) \left(1 - \frac{d_\infty^2}{\gamma^2} \right) 2 \frac{\gamma^2 - x_m d_\infty - d_\infty^2 \frac{T_{or}}{T_m}}{\gamma^2 - d_\infty^2} T_m + 2 \Theta(0,0) \frac{d_\infty^2}{\gamma^2} T_{or}$$

leading to – dropping the index m :

$$(T.18) \quad \Theta(x,y) = \Theta(0,0) \frac{\gamma^2 - x d_\infty}{\gamma^2}$$

And equation (12) becomes, now expliciting the parameters T_{or} , d_∞ :

$$(35) \quad T^*(T_{or}, d_\infty; x, y, T) = \Theta_{or} (\gamma^2 - x d_\infty) T - \Delta t_{or}$$

defining an adequate constant Θ_{or} .